

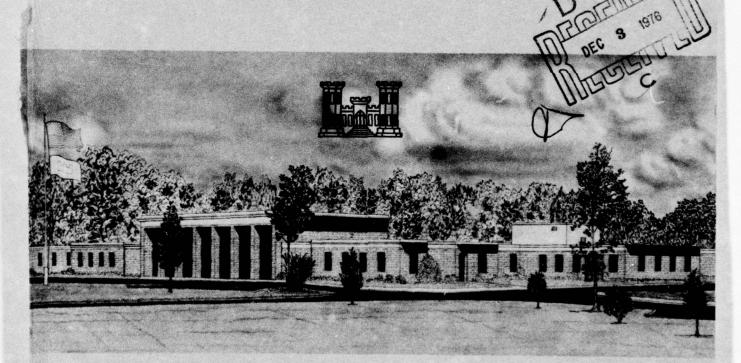




MISCELLANEOUS PAPER S-73-44

CONDITION SURVEY, FORBES AIR FORCE BASE, KANSAS

R. D. Jackson



June 1973

Sponsored by Office, Chief of Engineers, U. S. Army

Conducted by U. S. Army Engineer Waterways Experiment Station
Soils and Pavements Laboratory
Vicksburg, Mississippi

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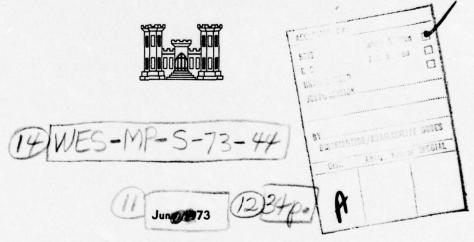


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by

10 R. D. Jackson, HoHoBaker G.D./Gilman



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Foreword

The study reported herein was conducted under the general supervision of the Engineering Design Criteria Branch, Soils and Pavements Laboratory, of the U. S. Army Engineer Waterways Experiment Station (WES), Vicksburg, Mississippi. Personnel involved in the condition survey were Messrs. R. D. Jackson, K. A. O'Connor, and S. R. Rowland, Jr., of the WES and Mr. H. H. Baker of the U. S. Army Engineer Division, New England (NED), Waltham, Massachusetts. The main portion of this report was prepared by Mr. Jackson under the general supervision of Messrs. J. P. Sale, R. G. Ahlvin, R. L. Hutchinson, and P. J. Vedros of the Soils and Pavements Laboratory. That portion of the study pertaining to frost action was carried out by the U. S. Army Cold Regions Research and Engineering Laboratory (CRREL), Hanover, New Hampshire, with the assistance of the Foundations and Materials Branch, NED. The section of the report concerning frost action was prepared by Mr. Baker and by Mr. G. D. Gilman of CRREL.

COL Ernest D. Peixotto, CE, was Director of the WES during the conduct of the study and preparation of the report. Mr. F. R. Brown was Technical Director.

Contents

Conversion Factors, British to Metric Units of Measurement

British units of measurement used in this report can be converted to metric units as follows:

Multiply	B y	To Obtain
inches	2.54	centimeters
feet	0.3048	meters
miles (U. S. statute)	1.609344	kilometers
square inches	6.4516	square centimeters
square feet	0.092903	square meters
miles per hour	1.609344	kilometers per hour
pounds (mass)	0.45359237	kilograms
pounds (force) per square inch	0.6894757	newtons per square centimeter

CONDITION SURVEY, FORBES AIR FORCE BASE, KANSAS

Authority

1. Authority for conducting condition surveys at selected airfields is contained in amendment to FY 1972 RDTE Funding Authorization (MFS-MC-5, 16 February 1972), subject: "Air Force Airfield Pavement Research Program," from the Office, Chief of Engineers, U. S. Army, Directorate of Military Construction, dated 18 February 1972.

Purpose and Scope

- 2. The purpose of this report is to present the results of a condition survey performed at Forbes Air Force Base (FAFB), Kansas, during 1-6 May 1972. The following three major areas of interest were considered in this condition survey:
 - <u>a.</u> The structural condition of the primary airfield pavements.
 - b. The condition of pavement repairs and the types of maintenance materials that have been used at this airfield.
 - c. Any evidence of detrimental effects of frost action to the pavement facilities.
- 3. This report is limited to a presentation of visual observations of the pavement conditions, discussion of these observations, and pertinent remarks with regard to the performance of the pavements. No physical tests of the pavements, foundations, or patching materials were performed during this survey.

Pertinent Background Data

General description of airfield

4. FAFB is located in Shawnee County, Kansas, approximately 5 miles* south of the city of Topeka. A vicinity map is shown in plates 1 and 2.

^{*} A table of factors for converting British units of measurement to metric units is presented on page vii.

5. In May 1972, the airfield facilities consisted of a NW-SE (13-31) runway, a NE-SW (21-03) runway, a series of taxiways, a large parking apron, three warm-up aprons, a washrack, a calibration hard-stand, and a series of hangar access aprons and taxiways. The NW-SE runway was 200 ft wide and 12,800 ft long; the NE-SW runway was 200 ft wide and 8,000 ft long; and the taxiways were at least 75 ft wide. The parking apron was 900 to 1,125 ft wide and approximately 3,760 to 5,300 ft long. A layout of the airfield is shown in plate 1. A pavement plan indicating the type pavement on each facility is shown in plate 2.

Previous reports

6. Previous reports concerning the airfield pavement facilities at FAFB are listed below. Pertinent data were extracted from them for use in this condition survey report.

a. Condition survey reports:

- (1) Ohio River Division Laboratories, CE, "Preliminary Report of Rigid Pavement Condition Survey of Topeka Air Base, Pauline, Kansas," August 1947, Cincinnati, Ohio.
- (2) , "Report of Rigid Pavement Condition Survey, Forbes Air Force Base, Pauline, Kansas," April 1951, Cincinnati, Ohio.
- (3) , "Report of Rigid Pavement Condition Survey, Forbes Air Force Base, Kansas," October 1957, and Addendum No. 1, October 1957, Cincinnati, Ohio.
- (4) _____, "Condition Survey Report, Forbes Air Force Base, Kansas," February 1961 (survey performed in 1960), Cincinnati, Ohio.
- (5) , "Condition Survey Report, Forbes Air Force Base, Kansas," January 1965, Cincinnati, Ohio.

b. Pavement evaluation reports:

- (1) U. S. Army Engineer Division, Missouri River, CE, "Pavement Evaluation Report, Topeka Airfield, Pauline, Kansas," December 1943, Omaha, Nebraska.
- (2) U. S. Army Engineer District, Kansas City, CE, "Airfield Evaluation Report, Forbes Air Force Base, Topeka, Kansas," December 1959, Kansas City, Missouri.

Design and construction history

- 7. Details of the construction history of the airfield pavements (extracted from the reports referenced in paragraph 6) are presented in table 1. Pavement thicknesses, descriptions, and other details are presented in table 2.
- 8. The original pavements, constructed during 1942 and 1943, were designed to support either 40,000- or 60,000-1b wheel loads. Pavements constructed or strengthened during the period 1952-55 were designed to support a 100,000-1b gear load supported on dual wheels spaced 37.5 in. center to center, with a tire contact area of 267 sq in. for each wheel.

Traffic history

9. A detailed traffic record for the airfield was not available; however, some approximation of the traffic can be made from the records that are available. From 1955-1965, the airfield was used primarily by B-47 and KC-97 aircraft. During the period January 1957-May 1957, an average of 304 cycles* per month of B-47 aircraft traffic and 147 cycles of KC-97 aircraft traffic were applied. For the period January 1958-June 1960, there were approximately 380 cycles of B-47 traffic and 85 cycles of KC-97 traffic applied. Assuming that the monthly level of traffic from 1955-1957 was the same as that for the first 4 months of 1957 and that the level from 1958-June 1965 was the same as that for the period January 1958-June 1960, the airfield would have sustained approximately 45,000 cycles of B-47 traffic and 12,000 cycles of KC-97 traffic. Since July 1965, the aircraft primarily using the airfield have been C-130's, C-135's, B-57's, and some transient aircraft. The average number of cycles per month for these aircraft have been as follows: C-130's, 2,900; C-135's, 263; B-57's, 800; and transient aircraft, 262.

Conditions of Pavement Surfaces

Pavement inspection procedure

10. The following procedure was used in conducting the inspection

^{*} A cycle of operation is one landing and one takeoff.

of the rigid pavements. Representative features were selected for detailed inspection. The features were then inspected slab* by slab, and the defects were recorded. The locations of the individual pavement features, the inspection starting points, and the directions in which the pavements were inspected (shown by arrows) are indicated in plate 1.

- 11. The results of the rigid pavement survey for those features that were inspected in detail are presented in table 3. This table shows a quantitative breakdown of the various types of defects and a condition rating for each pavement feature inspected in detail. The procedures used for determining the condition rating of a pavement are given in Appendix III of Department of the Army Technical Manual TM 5-827-3, "Rigid Airfield Pavement Evaluation," dated September 1965. Runways
- 12. The NW-SE (13-31) runway was in very good condition based on the percentage of slabs with no major defects; however, it was in a poor to failed condition based on the percentage of slabs with no defects. Combining the two ratings, the general condition of the runway would be fair. The condition of the NE-SW (03-21) runway, which is used primarily by C-130 aircraft for assault-type landings, was very good. This runway contained many slabs with longitudinal breaks, most of which were in the areas where the pavements had been overlaid. Neither of the runways had many slabs that were free of both major and minor defects. The minor defects consisted mostly of spalls, pop-outs, and map cracking. Several slabs were replaced in the center lanes of the interior portion of the NW-SE (13-31) runway in 1967.

Primary taxiways

13. The primary taxiway system is composed of taxiways 1, 3, and 3A. However, the portion of the NE-SW (03-21) runway between the NW-SE runway and taxiway 3 has been used extensively as a taxiway. Most of the defects in taxiway 1 that were noted in the 1965 report (see paragraph 6) had been corrected, and only one major defect remained. Several slabs were replaced in the center lane of taxiway 3 in 1966.

^{*} A slab is the smallest unit, containing no joints, of a given pavement feature.

The taxiway was in excellent condition at the time of the 1972 inspection. Taxiways 3 and 3A were in very good condition, with only 30 major defects noted in the two features.

Aprons

- 14. The parking aprons were in very good condition, even though the number of major defects had increased considerably since the 1960 survey. The distressed area along the east side of the apron north of taxiway 2 referred to in the 1965 condition survey was overlaid with asphaltic concrete (AC) in 1969. This area was in very good condition, even though there was some reflection cracking. Another area referred to in the 1965 survey, located along the east side of the parking apron between taxiways 3 and 4, was overlaid in 1969 with AC in some areas and with tar rubber (TR) in other areas. Even though some reflection cracking had begun in this area, it was in very good condition. In 1971, a portion of the parking apron was overlaid with TR to cover an area that contained a considerable amount of "D" cracking and a large number of spalls. The remainder of the parking apron was in good to very good structural condition, even though "D" cracking and pop-outs were prevalent (photos 1 and 2). Photo 3 shows AC patches at the corners of slabs of the parking apron. Portland cement concrete (PCC) patches along joints in the apron (photo 4) had been placed to repair areas that contained "D" cracking.
- 15. The remaining pavements not specifically mentioned above were in good to very good condition, even though many contained popouts.

Frost Action

Objectives of inspection

- 16. One member of the team inspected the pavement facilities for evidence of detrimental frost effects. The objectives of the inspection were to determine:
 - a. Any adverse effects of frost heave to the pavements during the winter months.

b. Any traffic-induced failures that might be related to thaw weakening of the subgrades or base courses.

Frost heave

- 17. The airfield pavements were inspected for surface irregularities indicative of differential frost heaving. This inspection, which was conducted on 3 May 1972, was several weeks subsequent to the frost-melting period at a time when evidence of frost heaving would not be apparent except in severe cases.
- 18. Base Civil Engineering Office personnel were queried regarding the development of undesirable pavement surface unevenness during the winter months. The consensus of the survey team was that the runway surface exhibited minor roughness detectable in an automobile at speeds of up to 60 mph. This unevenness appeared to be due to the slight settlement of certain pavement slabs rather than the result of frost heaving. The flexible shoulder pavements were smooth, and base personnel reported that no problems had been experienced with airfield pavement roughness. On the basis of the evidence available, it appears that none of the airfield pavements have been adversely affected by frost heave. The absence of detrimental differential frost heaving is believed to be due to uniform subgrade soil conditions.

Freezing indices

19. A design freezing index of 569 degree-days has been determined for FAFB. This value is based on temperature data from the Topeka, Kansas, Municipal Airport Weather Station and is the average of the three coldest winters in the past 30 years (1959-60, 1961-62, and 1962-63). Average daily temperatures for transition months at both ends of the freezing seasons were considered in this determination. Seasonal freezing indices for Topeka since the 1954-55 winter and the mean index are tabulated below. These values are based on average monthly temperatures.

Freezing Season	Freezing Index degree-days	Freezing Season	Freezing Index degree-days
1955-56	254	1957-58	209
1956-57	276	1958-59	322
	(Cont	inued)	

Freezing Season	Freezing Index degree-days	Freezing Season	Freezing Index degree-days
1959-60	410	1967-68	179
1960-61	130	1968-69	285
1961-62	552	1969-70	335
1962-63	437	1970-71	390
1963-64	266	1971-72	204
1964-65	133		
1965-66	189	30-year mean	105
1966-67	56		

These indices, being determined entirely from average monthly temperatures, generally reflect somewhat lower numerical values than do indices which consider average daily temperatures for the transition months. (The three values used to determine the design index are, for example, 558, 628, and 522 for 1959-60, 1961-62, and 1962-63, respectively.) The indices do, however, indicate the relative severity of the winters since the construction of the heavy-load pavements at FAFB. Since the three coldest winters in the past 30 years all occurred during this period, the pavements have experienced freezing conditions corresponding to the most severe recurrence frequencies that are considered in the Corps of Engineers design criteria.

20. For a design freezing index of 569 degree-days, a combined thickness of pavement and base course of 43 to 50 in., depending on base and subgrade water content and density and, to some extent, on pavement thickness, would be required to prevent subgrade freezing. Similarly, a combined thickness of 33 to 41 in. would be required to meet criteria for limited subgrade frost penetration design. The 16 to 32 in. of subgrade protection provided by the heavy-load pavements at FAFB are not adequate with respect to limited subgrade frost penetration design criteria; accordingly, performance must be compared with reduced subgrade strength design and evaluation criteria.

Groundwater

21. Evidence of high groundwater was observed in several of the pavement features, and base personnel reported that free water had been

encountered frequently under the slab or base course/subgrade interface during repairs.

Thaw weakening

- 22. The extent of thaw weakening of the subgrades and base courses could not be readily determined by inspection of the pavements. Pavement failures usually are repaired or otherwise corrected soon after they occur and consequently are not easily examined during a condition survey. However, even where an examination can be made, it is seldom possible to determine whether a failure resulted from thaw weakening or from pavement design deficiencies with respect to the "normal" period subsoil and traffic conditions. Some limited perception of thaw weakening effects can be gained, however, by examining the performance of certain pavement features with what might be expected in the light of applicable frost design criteria.
- 23. The heavy-load facilities at FAFB are all PCC pavements (some of which have been overlaid with AC or TR). As is stated in paragraph 20, reduced subgrade strength design and evaluation criteria are applicable for performance comparisons. These design methods require that rigid pavement slab thickness be determined on the basis of the frost-melting period subgrade modulus (kg). For the low design freezing index and uniform subgrade conditions at FAFB, current design criteria require a nonfrost-susceptible base course not less than 4 in. in thickness. The slab thicknesses are adequate for frost-condition operation of the design gear load and assembly (100,000 lb loaded on dual wheels, see paragraph 8); however, most of the pavements were placed directly on the subgrade. The principal aircraft using the airfield (B-47's, KC-97's, and C-130's, paragraph 9) have not overloaded these pavements during the frost-melting periods, and the small number of observed major structural defects (paragraphs 12-14) indicate that thaw weakening has not been a significant factor in pavement performance. No B-52 traffic has been reported at FAFB; however, operation of this aircraft would grossly overload most of the pavements, even for nonfrost conditions.

Maintenance

24. Due to the pop-outs and D-cracking, maintenance of the pavements at FAFB is generally conducted on a continuing basis. D-cracking usually progresses into corner, longitudinal, and transverse spalls. It was reported that maintenance costs for the period 1962-1967 averaged approximately \$600,000 annually. This maintenance consisted generally of joint sealing, slab replacement, and spall patching. A small AC overlay was placed in 1964. Maintenance costs since 1967 have been as fo lows:

Fiscal Year	Amount
1968	\$223,695
1969	284,271
1970	630,828
1971	90,178
1972 (10 months)	491,249

The higher maintenance costs shown for FY 1970 and 1972 resulted from placing overlays on the apron areas referred to in paragraph 14.

Evaluation

25. A summary of the pavement evaluation is presented in table 4. Previous evaluations were updated to include those aircraft that have been added to the Air Force inventory since the last survey and to exclude those that are no longer in the inventory. The evaluation is based on the pavement thickness, flexural strength (PCC), base and subbase thickness and strength, strength of the subgrade (CBR or k value), and the structural condition of the pavement.

Conclusions

26. The following statements summarize the findings of this inspection:

The following summarize the findings of this inspection: (1) The Portland Cement concrete (PCC)

- a. The PCC pavements were in good to excellent condition based on the percentages of slabs containing major defects; (2)
- b. D-cracking was very prevalent, with practically all slabs containing some degree of this defect; (3)
- c. Some reflection cracking was noted in the 1969 Ac overlay areas; and (4)
- d. Thaw weakening of the subgrade has not been a significant factor in pavement performance.

X

Table 1

	Length	ensions Width	Pavemen	-	Constru	otion	
Pavement Facility	ft	ft	in.	Туре	Year(s)	Agency	Remarks
N-S runway	6,525	150	10-8-10	PCC	1942	CE	Overlaid and now next of realist
		1,20			194	U.D.	Overlaid and now part of parking apron
NE-SW runway NW-SE runway	6,525	150 150	10-8-10	PCC PCC	1942 1942	CE	Overlaid; still in use
THE SECTION OF THE SE	0,200	130	10-0-10	Philip	194	CA	Rebuilt; now taxiway 3
Taxiway 1	3,075	50	9-7-9	PCC	1942	CE	Abandoned
Taxiway 2 Taxiway h	2,990	50	9-7-9	PCC	1942	CE	Abandoned
Taxiways 3 and 5	Varies	50	9-7-9	PCC	1942	CE	Now part of parking apron area Now part of parking apron area
Taxiways 6 and 7	Varies	50	9-7-9	PCC	1942	CE	Rebuilt
Taxiways 8, 9, and 10	Varies	50	9-7-9	PCC	1942	CE	Abandoned
Original parking apron	3,200	600	9-7-9	PCC	1942	CE	Overlaid
Parking apron extension No. 1	1426	600	9-7-9	PCC	1942	CE	Overlaid
Parking apron extension No. 2							
north Parking apron extension No. 2	550	600	11-8-11	PCC	1943	CE	Overlaid
south	1,287	480	11-8-11	PCC	1943	CE	Abandoned; 50-ft taxiway rebuil
All taxiways widened to 75 ft	Varies	25	9-7-9	PCC	1943	CE	
Parking apron, east side	3,200	75	9	PCC	1945	CE	Rebuilt as part of parking apro-
							taxiway
Taxiways 3, 4, and 5	Varies	75	9	PCC	1945	CE	Rebuilt
NE-SW runway	3,675	150	14	PCC	17/2	CE	Overlay
NE-SW runway	1,025	150	15	PCC	1952	CE	Overlay
NE-SW runway	Varies	25	16 and 18	PCC	1952	CE	50-ft widening
NE-SW runway	1,175	200	16	PCC	1952	CE	Rebuilt intersection at taxiway
NE-SW runway	1,475	500	16 and 18	PCC PCC	1952	CE	Extension
East warm-up apron Taxiway 2	3,800	375 75	18 18	PCC	1952 1952	CE	New construction
Taxiway 4 and fillet	Varies	Varies	16	PCC	1952	CE	New construction New construction
Parking apron	4,125	550	14 to 15	PCC	1952-53	CE	Overlay
Taxiway 5	900	75	14 to 15	PCC	1952-53	CE	Overlay
Parking apron (formerly part of N-S runway)	3,150	Varies	13 to 14	PCC	1954	CE	Overlay
Parking apron widening	3,800+	350 and 400	17	PCC	1954	CE	
South hangar access taxiway	1,200	75	17	PCC	1954	CE	
Taxiway 4	225+	75	17	PCC	1954	CE	
Taxiway 6, north portion	500+	75	17	PCC	1954	CE	
Taxiway 6, south portion	250+	75	18	PCC	1954	CE	
Parking apron extension	4,900+	900	17	PCC	1954-55	CE	
Taxiway 3, two sections	150	150	16	PCC	1954-55	CE	Part of old NW-SE runway
Taxiway 3, north section	2,300	75	17	PCC	1954-55	CE	
Taxiway 3, south section	3,700	75	17	PCC	1954-55	CE	
Taxiway 3A	1,400	75	17	PCC	1954-55	CE	
South warm-up apron	1400	500	17	PCC	1954-55	CE	
Taxiway 1	650	100	17	PCC	1955	CE	
North warm-up apron	400	200	17	PCC	1955	CE	
South hangar apron	300	175	17	PCC	1955	CE	
Calibration hardstand			17	PCC	1955	CE	
South hangar access aprons (3)	Varies	Varies	16	PCC	1955	CE	
North hangar access aprons (2) with taxiways	Varies	Varies	16	PCC	1955	CE	
NW-SE runway	12,800	200	16 and 17	PCC	1955	CE	Relocated
NW-SE runway, center 50 ft	500	50	24 and 22		1959	AF	Rebuilt
Taxiway 3, center 25 ft	1,600+	25	24 and 22		1959	AF	Rebuilt
	_						Redulit
Taxiway 2	450	25	24 and 22	PCC	1959	AF	
Blast pad reconstruction at NW-SE runway ends South apron	150	200	2 2(min)	AC AC	1962 1962	AF AF	Overlay
Parking apron	4,550	75	3	AC	1969	AF	Overlay of 17" PCC
Parking apron	1,100+	Varies	3	AC.	1969	AF	Overlay of 13/8 and 17" PCC
Parking apron	2,750	250	3	TR	1969	AF	Overlay of 17" PCC
Parking apron	1,225	900		m	3.0071		Overlay of 17" PCC
		825	3	TR	1971	AF	interless of 17 PCC

Note: CE denotes Corps of Engineers; AF denotes Air Force.

Table 2

SUMMARY OF PHYSICAL PROPERTY DATA

FACILITY				OVERLAY PAVEMENT			PAVEMENT	-		BASE	1	SUBGRADE		GENERAL
Forbes AFB, Kansas FACILITY NUMBER AND IDENTIFICATION	LENGTH	WIOTH FT	THICK.	DESCRIPTION	FLEX. STR PSI	THICK.	DESCRIPTION	FLEX. STR PSI	THICK.	CLASSIFICATION	0 0 ×	CLASSIFICATION	9 8 ×	OF AREA CONSIDERED
RIA NW-SE runway; center 50 ft of lat 229 ft, NW end	225	20				32	Portland cement concrete	720	Ø	Crushed stone or crushed gravel	75	Cley (01-01)		Very pood
R2A WW-SE runway; center 50 ft of next 275 ft, NW end	275	28				25.	Fortland cement concrete	720	9	Crushed stone or crushed gravel	75	Clay (CL-CH)		2002 (Las.)
R3A NW-SE runway; lst 500 ft, NW R15D eni, 75-ft-wide section each side	000	75				17	Fortland cement concrete	720				clay (ct.cH)	200	Very good
RMB MM-SE runway; 2nd 500 ft, NW end	2005	500				17	Fortland cement concrete	720				(0149 (01-00)	7. F. 25.5	Yery rood
850 MW-SE numway interior	10,000	500				36	Fortland cement concrete	720				Clay (CL-CS)	15 × 255	Very pool
R6C W-SE number interior	800	500				17	Fortland cement concrete	720				Clay (CL-CK)	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	(ex- 100)
R/B NW-SE runway; 2nd 500 ft, SE end	200	500				1.7	Fortland cement concrete	720				C187 (CL-CH)	25 A	Very good
BBA NW-SE runway; let 500 ft,	200	500				17	Portland cement concrete	720				(NO-13) AR13	1,485	Exceller
R9A NE-SW numway; lst 500 ft, NE end	500	200				18	Fortland cement concrete	720	-3	Sand (SP)	X 75	Clay (CL-CH)		Excellent
RIOB NE-5W runway: 2nd 500 ft, NE end	900	500				18	Fortland cement concrete	720	a	Sand (3P)	75 k 123	Cley (CL-CH)		Expellent
Rilc NE-SW runway interior	2,200	200				76	Fertland cement concrete	720	-3	(SP)	7. ×	Clay (CL-CH)		3000
S120 NE-SW runsay interior	Varies	150	14 to 15	Fortland cement concrete hg = 15.62	720	c c	Fortisnd cement concrete 10-8-10					Clay (CL-CH)	07	Bood
RLW NE-GW runway; 2nd 500 ft,	200	150	15	Portland cement concrete hg = 16.55	720	at)	Portland cement concrete 10-8-10					Clay (cL-CH)	07 2	Excellent

(1 of 4 spects

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Table 2 Continued

SUMMARY OF PHYSICAL PROPERTY DATA

FACILITY			H		OVERLAY PAVEMENT			PAVEMENT			BASE		SUBGRADE		GENERAL
Forbes AFB, Kansas FACILITY NUMBER AND IDENTIFICATION	N LENGTH	H WIDTH		THICK.	DESCRIPTION	FLEX. STR PSI	THICK.	DESCRIPTION	FLEX. STR PSI	THICK.	CLASSIFICATION	0 0 ×	CLASSIFICATION	9 8 ×	CONDITION OF AREA CONSIDERED
RILA NE-SW runway; let 500 ft, SW end	9005	150	15	H O A	Fortland cement concrete h _E = 16.55	720	α5	Fortland cement concrete 10-8-10					Olay (CL-CH)	50.5	Excellent
TlA Taxiway l	650	100					17	Fortland cement	720				Clay (CL-CH)	8	excellent
12A Taxiway 3 Taxiway 3A	Varies 1,400	Varies 75	100				17	Portland cement concrete	720				Clay (ct.cif)	× 3.	Excellent Very good
TSA Taxiway 3	1,800±	52					57	Fortland cement concrete	720	9	Crushed stone	75 K + 83	Clay (CL-CH)		Sketllent
ThA Thainny 3, two sections Fillet on taxiway h	150 Varies	150 Varies	99				16	Fortland cement concrete	720				Clay (CL-CH)	8 ×	Excellent
TSA Taxiway 2	3,800	25					18	Portland cement concrete	720	.7	Sand (SF)	75 * 4* 25	Clay (CL-CH)		Very good
TGA TRACKRY 5	006	22		14 to 15 P	Fortland cement concrete $h_{\rm E}=15.26$	720	-	Fortland cement concrete 9-7-9					Clay (CL-CH)	k rw2f	Sood
T7a Taxiway 6	\$000	12					17	Fortland cement concrete	720	æ	Sand (SP)	50 See	CINY (CL-CH)		Skellent
18A Textway 6	250 1	52					18	Fortland cement concrete	720	-3	Sand (SP)	23	Chay (ct-cn)		xeller
19A Apron access taxiway	1,400	52					17	Portland cement concrete	720	æ	Crushed stone	75 kg=50	Clay (CL-OH)		Nery good
TIOB Apron access taximay	1,200	72					17	Fortland cement concrete	720				(נוסא (כד-טא)	× × ×	Very good
TILA Taxiway L	225	75	m	- A.	Asphaltic concrete hy = 19.00		17	Fortland cement concrete	720				Clay (CL-CH)	5 × 5	
TIZA Taximy 4	28.5	75	pri .	4.4	Asphaltic concrete hg = 17.89		16	Fortland cement concrete	720				Clay (CL-CH)	14 P. 1859	
Alle Farking apron	Varies	Varies	## ## ## ## ## ## ## ## ## ## ## ## ##				11	Fortland cement	780				ciay (ct-cm)	£ %	Tery good

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2 of 4 sheets

Table 2 (Continued)

SUMMARY OF PHYSICAL PROPERTY DATA

	FACILITY				OVERLAY PAVEMENT			PAVEMENT	-		BASE	T	SUBGRADE	T	GENERAL
E 63	OLDES AFF, EN1595 FACILITY NUMBER AND IDENTIFICATION	LENGTH	#IDTH FR	THICK.	DESCRIPTION	FLEX. STR PSI	THICK.	DESCRIPTION	STR PSI	THICK.	CLASSIFICATION	# 8 ×	CLASSIFICATION	55×	OF AREA CONSIDERED
-	Parking apron	4,125	550	14 to 15	Fortland cement concrete h _E = 15.26	720	7	Fortland cement concrete 9-7-9					Clay (CL-CH)	97 J.	Very cool
	Parking apron and taxiway	1,225 h,450 Varies	825 250 3 Varies 3 75	തതത്ത	Tar rubber (1,010,625 sq.ft) Asphalite concrete h _E = 19.00		17	Fortland cement concrete	720				Clay (CL-CH)	8	
	Farking apron	Varies	22	6	Tar rubber h _E = 18.93		17	Fortland cement comerete	720				Clay (cL-cH)	LO 2 4 425	
	North wars-up apron South wars-up apron South hangar apron	300 000	200				17	Fortland cement concrete	720				Clay (CL-CH)	2	Soog Very good
	East Marm-up apron	200	375				18	Fortland cement concrete	720	2	Sand (SP)	75 X-45	Clay (CL-CH)		\$000
	South hangar access apron	Varies	Varies				91	Fortland cement	720				(OF-CH)	75 11,425	
	North bangar access aprons and taxiway	Varies	Varies				36	Fortland cement	720				Clay (CL-CH)	75 K ₁ #25	
89	Parking apron	3,150	Varies	3 over 13	Tar rubber over portland cement concrete hg = 14.77	720	œ	Fortland cement concrete 10-8-10					Clay (CL-CH)	60 × ×	
A108	South aprom	006	175	N	Asphaltic concrete		0.	Fortland cement	720				Olay (CL-CH)	75 R + *25	
Allc	Calibration hardstand and taxiway 4	Varies	Varies				17	Fortland cement	720				Clay (CL-CH)	75 7.4.65	
AIZB	Ferking apron	004		3 over 13	Asphaltic concrete/ portland cement concrete h _E = 14.77	720	8	Fortland cement concrete 10-8-10					C18, (CL-CH)	75	
я16х	MR-5M runway overrun, ME end	1,000	200				Ĉ.	Double bituminous surface treatment					C1Ay (C1CH)	us.	
	RITX NE-SW runway overrun, SW end	1,000	200				c	Double bituminous surface treatment					Clay (CL-CH)	45	
	R18% IM-SE runway overrun, SW end	150	200				O4	Asphaltic concrete		99	Crushed stone base Granular subbase		Clay (CL-CH)	.10	

(3 of 4 spect

Table 2 (Continued) SUMMARY OF PHYSICAL PROPERTY DATA

DATE:	May 1972				SUI	SUMMARY OF	Y OF	DATA	- 1	RIGID PAVEMENT CONDITION SURVEY	AVEN	ENT	CONDI	NOIL	SURV	EY					AIRFIELD:	Forbes
	FEATURE	St. AB	APPROX	PAVE.					NO. C	OF SLA	as co	NIAIN	SLABS CONTAINING INDICATED DEFECTS	CATE	D DEFE	CTS					20 %	5 %
ý	DESIGNATION	SIZE	NO. OF SLABS	ž ž	-	1	/	٥	*	× ,	8	5	7	7	•	Σ	۵	0	U	۵	067EC15	WAJOR DIFECTS
RIA R2A R3A	NW-SE runway; lst 500 ft, NW end	25 by 25	100	22	67		н	н		-	н	-	an)	2	13				п		See	6'96
яфв	NW-SE runway; 2nd 500 ft, NW end	25 by 25	160	17	6		н	1			7		80	2	13				п			8.9
RSC	NW-SE runway interior	25 by 25	3258	16	18	CV .	10	12			23	10 158		30 258	8				13			97.3
Réc	NW-SE runway interior	25 by 25	256	17	9		Т	П			cu	2	15	m	25 1				-			97.5
R/7B	NW-SE runway; 2nd 500 ft, SE end	25 by 25	160	17	C)							-	4	-	æ		_					98.0
38A	NW-SE runway; 1st 500 ft, SE end	25 by 25	160	17	m.						rH	-	8	0	13				м			88
R9A	NE-SW runway; lst 500 ft, NE end	25 by 25	160	18	15	7	Н	н	-		1		N	9	19				ri			98.7
RIOB	NE-SW runway; 2nd 500 ft, NE end	25 by 25	160	18	15	4	٦	Т			1	п	O.	9	19				ч			98.7
RIIC	NE-SW runway interior	25 by 25	3128	16	589	89	70	22	N		17	16 4	b3 112	366	9				98			87.5
8138	NE-SW runway; 2nd 500 ft, SW end	25 by 25	160	15/10- 8-10 18	15	6	ч	н			п	н	a	6 1	19				п			98.8
ag.	REMARKS: Practically all slabs contained mathat that did not contain other defects.	all slabs	s contai	contained map cracking and one ther defects.	crack	ing and		or more	or more pop-outs; "D" cracking was evident in practically all slabs	nts; "	D" cra	cking	was ev	ident	in pra	ctica	t1s vt	slabs.				
LEG	LEGEND: LONGI TRANS NO DIAGO CORNE STATI	LONGITUDINAL CRACK TRANSVERSE CRACK DIAGONAL CRACK CORNER BREAK SHATTERED SLAB	ACK ACK .URE		\$ 0 h → 7 +	SHRINKAGE CRASCALING SPALL ON TRASPALL ON LON CORNER SPALL SETTLEMENT	SHRINKAGE CRACK SCALING SPALL ON TRANSVERSE JOINT SPALL ON LONGITUDINAL JOIN CORNER SPALL	SVERSE	SHRINKAGE CRACK SCALING SPALL ON LONGITUDINAL JOINT CORNER SPALL SETTLEMENT		2000	MAP CRACKING PUMPING JOINT POP-OUT UNCONTROLLED CONTRACTION O	MAP CRACKING PUMPING JOINT POP-OUT UNCONTROLLED CONTRACTION CRACKING	ž								

AFB.		CONDITION	Excel-	Excel-	Excel.	Fery good	Very	Good	Excel-	Very	Very				ets)			
AIRFIELD: Forbes AFB,		MAJOR DEFECTS	8 8	99.1	88	8.	7.36	9.68	98.4	6.49	9: F				of 3 sheets)			
AIRFIELD:	50 %	NO DEFECTS	See												(5 0			
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		U	п	1	П					1	25							
		0											Ť					
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ΕΥ	CTS	Σ																
RIGID PAVEMENT CONDITION SURVEY	NO. OF SLABS CONTAINING INDICATED DEFECTS	•	0	m	2	- 5	10											
NOIL	CATE	7	19			41	16	27	34	8	476			š				
OND	AG IND	7	un.		cu	-	80	13	2	22	83			MAP CRACKING POURPING JOINT POP-OUT POR-OUT CONTRACTION CRACK TO* CRACKING				
NT	TAINI	ה	2		-# Ci			23 3	m	15	35 86			MAP CRACKING PUMPING JOINT POP-OUT UNCONTROLLED CONTRACTION C				
VEME	S CON	S	1		ļ		6	N		0	1			2000				
D PA	SLAB	*								10	56							
- RIG	NO. OF	×			-						đ			TNIOC				
ATA		*	1			20	01					-		SHRINKAGE CRACK SCALING SPALL ON TRANSVERSE JOINT SPALL ON LONGITUDINAL JOINT CORNER SPALL SETTLEMENT				
SUMMARY OF DATA		٥			П	u v	10			2 11	24 110			CRACK TRANSVI LONGITU ALL				
AARY		/	m		ω		н	10	CV.	N	41	-		SHRINKAGE CRACK SCALING SPALL ON IRANS\ SPALL ON LONGIT CORNER SPALL				
SUMA		_	15	п	ET .	CU.	11	23		m	+							
	ř.	<u> </u>					-	-	17 and 18		to 252 9-			\$ 0 D 3 7 0				
		ž Ž	15/10- -8-10 18		17 24 14 to 15 16	17	18	14 to 15/7		-	14 to 15/9- 7-9							
	APPROX	SLABS	160	108	1338	200	1967	245	152	349	7963			CR ACK				
	SLAB	SIZE FT	25 by 25	25 by 25	25 by 25 25 by 25 15 by 25	25 by 25	25 by 25	25 by 25	12-1/2 by 25 25 by 25	25 by 25	25 by 25			LONGITUDINAL CRACK TRANSVERSE CRACK DIAGONAL CRACK CORNER BREAK SHATTERED SLAB				
May 1972	FEATURE	DESIGNATION	NE-SW runway; 1st 500 ft, SW end	Taxiway l	Texiway 3	Taxiway 3A	Taxiway 2	Taxiway 5	Тахімау б	Apron access taxiway	Parking apron		RK S:	-1/4**	2004			
DATE:		, o	R14A	TIA	TEA TEA TEA TABLE THA		TSA 1	TGA	T7A T	T9A A	Alb F		REMARKS:	LEGEND	WES FORM NO.			
61			R	E	T E E	IS	17.5	IĆ	CO	PY RMI	AVA		BLE TO	DDC DO	S NO			

FEATURE State St	A	DATE: May 1972	1				SUM	SUMMARY OF		DATA		GID P	AVEN	FNT	RIGID PAVEMENT CONDITION SURVEY	NOITI	SUR	VEY					AIRFIELD:	D: Forbes AFB, Kansas	AFB,
A38 North without Cauch Canada Salary Canada Cauch Canada Salary Canada Cauch Canada Salary Canada C		FEATURE	84.48		-	, K	1				Ö		BS CC	ONTAIN	N SNI	DICAT	ED DE	FECTS					\$ 00 St. A65		
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ASS North wareup 25 by 25 133 17 3 3 1 6 3 3 1 1 7 7 9 9 1 9 1 9 1 7 7 9 9 1 9 1 9 1	A2	-		25				61	775		10		1	-	-	-	cy			-		CVI	See		1
ASS South ware-up					-	7	m	m	н	9			67		m		7							98.1	
A care a part and the care A care a part				1	-	7	rt	-		7	-		CV CV			-	m		-	-	-	d		8.	
ASS South hanger 25 by 25 399 16 21 2 4 3 14 24 5 43 89.55			25 by		-		61	m	2	5			7	95			-					-		85	-
LONGITUDINAL CRACK		-	25	25	-		51	cu	4	m			14		†12	-	8					6		8.3	1
LONGITUDINAL CRACK					-			-						-				-							
LONGITUDINAL CRACK				-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			-
LONGITUDINAL CRACK																-	-	-	-						
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LONGITUDINAL CRACK						-			-	-		-		-	-	-	-	-	-	-	-	_			
LONGITUDINAL CRACK	ä	MARKS:								1		1		-		-	-								
TRANSVERSE CRACK SCALING SPALL ON TRANSVERSE JOINT CORNER BREAK SHALL ON TRANSVERSE JOINT CORNER SPALL CORNER S	1 3	-	LONGITUDINAL	L CRACK		1		INKAGE	CRAC				1	AP CRA	CKING										
CORNER BREAK SPALL ON LONGITUDINAL JOINT C SHATTERED SLAB J CORNER SPALL D KEYED JOINT FAILURE STITLEMENT		1/	TRANSVERSE DIAGONAL CA	CRACK		רו נט		ALING LL ON	TRANS	VERSE	TNION			UMPING OP-OUT	TNIOC										
KEYED JOINT FAILURE SETTLEMENT			CORNER BRE	AK SLAB		-		INFR SP	LONGI	UDINAL	LOINT			NCONTRAC	TION CR	ACK									
			KEYED JOINT	FAILURE		•		TLEME	ż																

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, o		200				TRIC	THE AND	EMENT				BICYCLE	
NO.	FEATURE	VEMENT	SINGLE 100-PSI	SINGLE 100-SQ-IN,	SINGLE 241-5Q-IN.	T# 28-IN, C-C Z26-5Q-IN, CONTACT AREA	SINGLE TANDEM 60-IN. SPACING 400-50-IN.	TH MAIN C.C. 267.50-IN. CONTACT AREA	T# 44-3N C-C 630-59-4N. CONTACT AREA	7 KIN TANDEM 33 IN * 46 IN 206-50-IN.	CSA GEAR CONFIGURATION	TRIN TRIN SPCG 31-42-37 267-50-18.	REMARKS
	DESIGNATION			2		EACH TINE	CONTACT AREA	EACH TIME	7	EACH TIRE	on.	10	
NIA N	WM-SE runway; center 50 ft of 1st 225 ft, NW end	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000+	200,000+	330,000+	230,000+	380,000+	800,000+	430,000	
R2A M	NW-SE runway; center 50 ft of next 275 ft, NW end	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000+	200,000+	330,000+	230,000+	380,000+	800,000+	410,000	
R3A M	NM-SE runway; lst 500 ft, NW end	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000	200,000+	205,000	230,000+	330,000	740,000	230,000	
RAB M	NW-SE rumway; 2nd 500 ft, Nw end	Capacity Frost capacity	155,000+	85,000+ 85,000+	155,000+	3,85,000	200,000+	245,000	230,000+	380,000+	800,000+ 740,000+	310,000	
R5C M	WW-SE runway interior	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000+	200,000+	295,000	230,000+	380,000+	800,000+	390,000	
R6C N	NW-SE runway interior	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000+	200,000+	320,000	230,000+	380,000+	800,000+	330,000	
R7B M	NW-SE runway; 2nd 500 ft, SE end	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000	200,000+	245,000	230,000+	350,000+	800,000+	310,000	
R84 M	NW-SE runway 1st Capacity 500 ft 31 end Frost ca	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000	200,000+	205,000	230,000+	330,000	800,000+ 740,000	230,000	
R9A M	NE-SW runway; 1st 500 ft, NE end	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000+	200,000+	220,000	230,000+	350,000	800,000+	320,000	
RIOB N	NE-SW runway, 2nd 500 ft, NE end	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000+	200,000+	270,000	230,000+	380,000+	800,000+	340,000	
RIIC N	NE-SW runway interior	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000+	200,000+	295,000	230,000+	390,000+	800,000+	390,000	

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Table 4 (Continued) SUMMARY OF PAVEMENT EVALUATION

NAME	NAME OF AIRFIELD. Forb	Forbes AFB, Kansas	7	LOAD-CARRYING CAPACITY IN LB OF GROSS PLANE LOAD FOR INDICATED LANDING GEAR TYPES AND CONFIGURATIONS	S CAPACITY IN	LB OF GROSS	PLANE LUMUT	OR HANDAMAN	L'Alternation was				
M	MONTH: May YR: 1972	1972				TRIC	TRICYCLE ARRANGEMENT	EMENT				BICYCLE	
	FEATURE	VEMENT	SINGLE 100-PSI TIRE PRESSURE	SINGLE 100-5Q-IN. CONTACT AREA	SINGLE ZAT-SQ-IN. CONTACT AREA	TW 28-IN. C.C. 226-50-IN. CONTACT AREA	SINGLE TANDER 60-IN SPACING 400-50-IN	TW 30-IN C-C 25 - Sto-IN CONTACT AND A	TW 64-IN, C-C 630-50-IN CONTACT AREA	THIN TANDEM 33 IN THE IN. 208-50-IN. CONTACT AREA	C-5A GEAR CONFIGURATION	SPEC DIAZIN SPEC DIAZIN SPISONA CONTACT AREA	REMARKS
ŏ	DESIGNATION	USE	-	2	6	4	8	9	7	EACH TIME	6:	10	
RI2C	NE-SW runway	Capacity	155,000+	85,000+	155,000+	220,000+	200,000+	255,000	+000,085	380,000+	800,000+	320,000	
	interior	Frost capacity	155,000+	85,000+	155,000+	215,000	200,000+	235,000	\$30,000+	360,000	800,000+	295,030	
R13B	+	Capacity	140,000	85,000+	155,000+	190,000	+000,005	205,000	230,000+	330,000	800,000+	265,000	
	2nd 500 ft, SW end	Frost capacity	135,000	85,000+	155,000+	175,000	500°,000+	190,000	230,000+	290,000	800,000+	240,000	
RILAA	1	Capacity	140,000	85,000+	145,000	190,000	200,000+	175,000	220,000	280,000	800,000+	310,000	
	1st 500 ft, SW end	Frost capacity	135,000	85,000+	145,000	175,000	500,000+	175,000	220,000	280,000	800,000+	240,000	
TIA	Taxiway 1	Capacity	155,000+	85,000+	155,000+	220,000	200,000+	205,000	230,000+	330,000	800,000+	295,000	
		Frost capacity	140,000	85,000+	155,000+	185,000	+000,005	165,000	200,000	255,000	740,000	230,000	
TZA	Taxiway 3	Capacity	155,000+	85,000+	155,000+	220,000	200,000+	205,000	230,000+	330,000	800,000+	000,763	
	Taxiway 3A	Frost capacity	140,000	85,000+	155,000+	185,000	200,000+	165,000	200,000	255,000	740,000	230,000	
T3A	Taxiway 3	Capacity	155,000+	85,000+	155,000+	220,000+	200,000+	330,000+	230,000+	380,000+	800,000+	480,000	
		Frost capacity	155,000+	85,000+	155,000+	220,000+	200,000+	330,000+	£30,000+	380,000+	800,000+	440,000	
THE	Taxiway 3,	Capacity	145,000	85,000+	150,000	200,000	200,000+	185,000	230,000+	310,000	800,000+	270,000	
	two sections Fillet on Taxiway 4	Frost capacity	130,000	85,000+	130,000	170,000	200,000+	155,000	190,000	235,000	000*069	(8)	
TSA	Taxiway 2	Capacity	155,000+	85,000+	155,000+	220,000+	200,000+	220,000	230,000+	350,000	800,000+	320,000	
		Frost capacity	155,000	+000,58	155,000+	200,000	500,000+	220,000	£30,000+	350,000	900°000+	200,000	
TGA	Taxiway 5	Capacity Frost capacity	125,000	85,000+	130,000	170,000	200,000+	155,000	195,000	250,000	740,000	(a) (a)	
T7A	Taxiway 6	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000	200,000+	205,000	230,000+	330,000	800,000+ 745,000	230,000	
TSA	Taxiway 6	Capacity Frost capacity	155,000+	85,000+	155,000+	200,000+	200,000+	220,000	230,000+	350,000	800,000+	320,000	
T9A	Apron access tardway	Capacity Frost capacity	155,000+	85,000+	155,000+	220,000	200,000+	205,000	230,000+	330,000	800,000+	295,000	

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(2 of 4 sheets)

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Table 4 (Continued) SUMMARY OF PAVEMENT EVALUATION

MONT	MONTH: May YR: 1972	1972	-			TRUC	TRICYCLE ARRANGEMENT	EMENT				BICYCLE	
	FEATURE	PAVEMENT	SINGLE 100-95	SINGLE 100-SQ-IN.	SNOLE 241-3Q-IN.	TW 28-IN, C.C. 226-SQ-IN. CONTACT AREA	SPECEE TANDEM COLN. SPACING 400-504N.	TA 35 JN. C.C. 2019Q-IN CONTACT AREA	T* 44-IN. C-C 410-50-IN. CONTACT # RDA	TWO TANDEM	CAN	SPEC PACKET SPECIAL SP	REMARKS
NO.	DESIGNATION	asa asa	1	2	3	CACH TIRE	CONTACT AREA	-	EACH TIRE	CACH TIME	0)	TACH TIME	
T108 A	Apron access	Capacity	155,000+	85,000+	155,000+	220,000+	+000,000	330,000+	230,000+	380,000+	800,000+	310,000	
	taxiway	Frost caparity	140,000	85,000+	155,000+	185,000	+000,00%	200,000	230,000+	310,000	800,000+	000,055	
TIN T	Taxivay 4	Capacity	155,000+	85,000+	155,000+	4000,022	+000,009	235,000	230,0004	380,000	800,000+	360,000	
-		Frost capacity	155,000+	85,000+	155,000+	220,000+	+000,00G	235,000	£30,000+	345,000	800,000+	295,000	
TISA T	Taxiway 4	Capacity	155,000+	+000,38	155,000+	220,000+	200,000+	215,000	230,000+	350,000	+000°009	330,000	
		Frost capacity	155,000	+0000,88	155,000+	200,000	-H000,009	215,000	E30,000+	350,000	800,000+	270,000	
ALIB Pr	Parking apron	Capacity	155,000+	+000,28	155,000+	220,000	+000,009+	330,000+	930,000+	380,000+	800,000+	210,000	
		Frost capacity	140,000	+000,58	155,000+	185,000	200,000+	200,000	230,000	310,000	800,000+	250,000	
A2B Ps	Parking apron	Capacity	125,000	85,000+	155,000	170,000	200,000+	185,000	225,000	290,000	800,000+	835,000	
		Frost capacity	115,000	85,000+	145,000	155,000	+000,002	170,000	205,000	260,000	740,000		
A3B Fe	Parking apron	Capacity	155,000+	85,000+	155,000+	220,000+	200,000+	280,000	230,000+	380,000+	800,000+	350,000	
(C)	and taxiway	Frost capacity	155,000+	85,000+	155,000+	220,000+	4000,005	240,000	230,000+	350,000	+000,008	300,000	
A4B TP8	Farking apron	Capacity	155,000+	85,000+	155,000+	220,000+	200,000+	250,000	230,000+	380,000	800,000+	320,000	
		Frost capacity	155,000+	85,000+	155,000+	220,000	200,000+	235,000	530,000+	34.0,000	800,000+	290,000	
A5B Me	North and south	Capacity	155,000+	85,000+	155,000+	220,000	200,000+	330,000+	230,000+	380,000+	800,000+	310,000	
10 10	south hangar	Frost capacity	140,000	85,000+	155,000+	185,000	200,000+	200,000	230,000+	310,000	800,000+	250,000	
A6B Ba	East warm-up	Capacity	155,000+	85,000+	155,000+	220,000+	200,000+	270,000	830,000+	380,000+	-800,008	340,000	
8	apron	Frost capacity	155,000	85,000+	155,000+	200,000	200,000+	220,000	230,000+	320,000	800,000+	270,000	
A7B Sc	South bangar	Capacity	145,000	85,000+	155,000+	200,000	200,000+	220,000	230,000+	360,000	800,000+	290,000	
25	access apron	Frost capacity	125,000	85,000+	155,000	170,000	+000,009	190,000	6.30,000	595,000	800,000+	240,000	
ASB No	North hangar	Capacity	145,000	85,000+	155,000+	200,000	200,000+	220,000	230,000+	360,000	800,000+	290,000	
it it	access aprons and taxiway	Frost capacity	125,000	85,000+	155,000	170,000	+000,000	190,000	230,000	595,000	800,000+	240,000	
P.	Parking apron	Capacity	120,000	85,000+	145,000	160,000	+000,009	175,000	215,000	280,000	800,000+	(8)	
		Frost capacity	110,000	85,000+	135,000	150,000	200,000+	165,000	200,000	955,000	730,000	(8)	

EDITION OF AUG 1960 IS OBSOLETE.

(3 of 4 spects

Table 4 (Continued) SUMMARY OF PAVEMENT EVALUATION

COPY AVAILABLE TO DDG DOES NOT PERMIT FULLY LEGIBLE PRODUCTION



Photo 1. "D" cracking on parking apron



Photo 2. Pop-outs on parking apron



Photo 3. AC repairs at slab corners of parking apron



Photo 4. PCC repairs along joints in parking apron

